

HBBA Study: Conclusions

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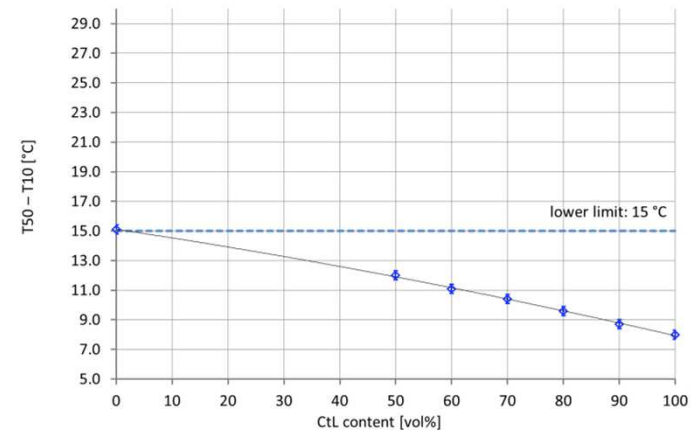
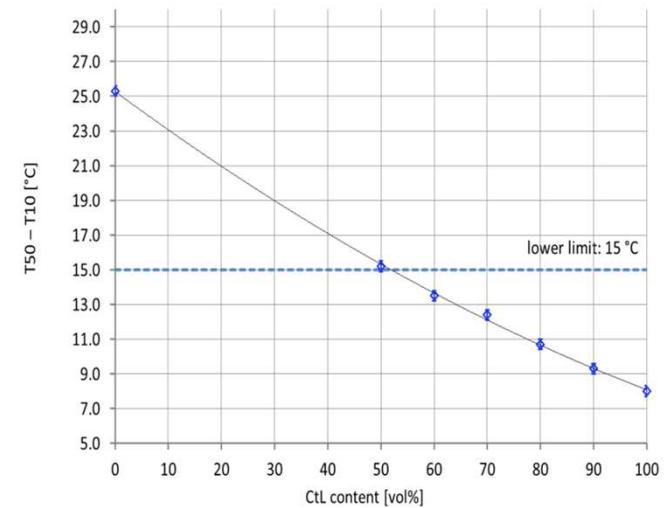


General remark

- Main output of HBBA study is to provide data base
 - Facilitates practical blending
 - Will also assist scientific research
- Data base has been created
 - Detailed data available in appendix to HBBA report
 - Made generally accessible via BioJetMap
- In addition to data base, various insights gained
- Key conclusions outlined in this presentation

Constraining factors for FT and HEFA

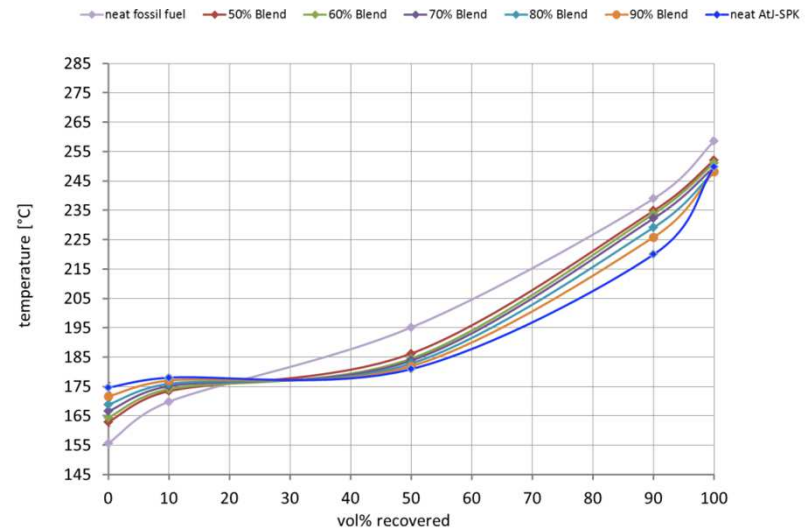
- Constraining factors for FT SPK
 - Distillation curve gradients, particularly T50-T10
 - For three conventional kerosene, limited to some 50% blend ratio
 - For one conventional kerosene, limited to some 25% blend ratio
 - For one fuel with narrow distillation curve, blends off-spec at all ratios
 - Aromatics: Maximum blend ratio achievable 40% - 70%
 - Density: Maximum blend ratio achievable 50% - 75%
- Constraining factors for HEFA SPK
 - Aromatics: Maximum blend ratio achievable 40% - 70%
 - Density: Maximum blend ratio achievable 40% - 70%



Two examples of T50-T10 for blends with CTL

Constraining factors for SIP and ATJ-SPK

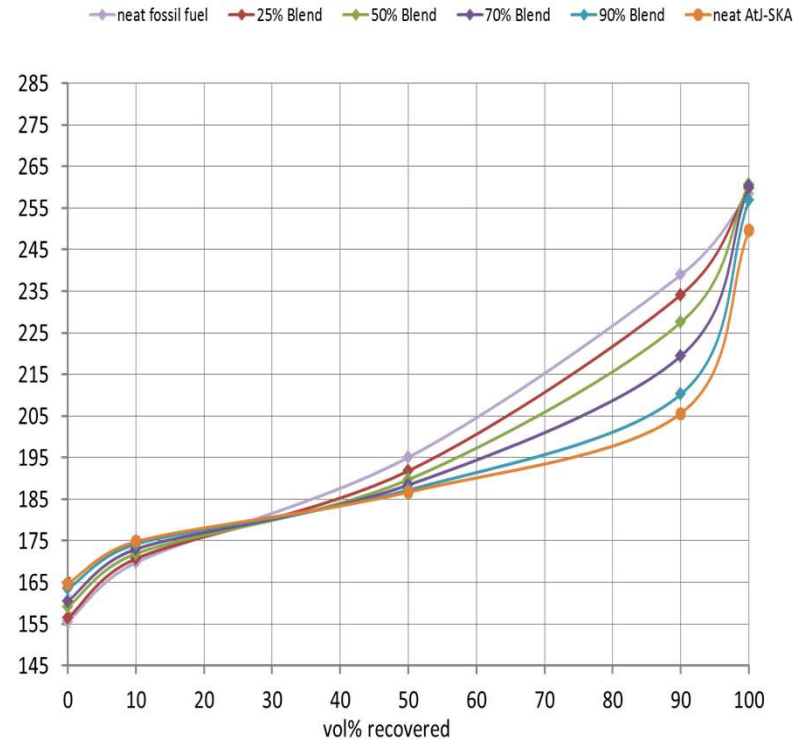
- Constraining factors for SIP fuel
 - Viscosity at -40°C: Maximum in spec blend ratio achievable ca. 30%
 - Aromatics: Maximum blend ratio achievable 40% - 70%
 - Density only constraining factor at blend ratios well above 80%
- Constraining factors for ATJ- SPK
 - T50-T10
 - Only low blend ratios achievable, max. 30%
 - For kerosene with narrow distillation curve, blends off-spec at all ratios
 - Aromatics: Maximum blend ratio achievable 40% - 70%
 - Density: Maximum blend ratio achievable 40% - 70%



Distillation curve of ATJ-SPK and of blends

Constraining factors for ATJ-SKA and CH kerosene

- Constraining factors for ATJ-SKA
 - Distillation curve only constraint
 - Both T50-T10 and T90-T10
 - Maximum blend ratio between zero and 70%
 - For all other parameters, ASTM D7566 already met by neat fuel
- Constraining factors for CH kerosene
 - None
 - All ASTM D7566 parameters already met by neat fuel



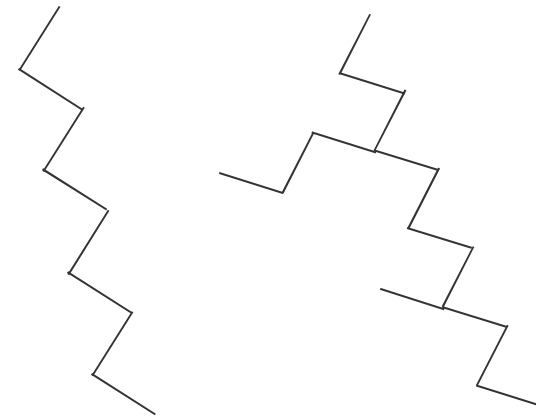
Distillation curve of ATJ-SKA and of blends

Observations on distillation curve gradient

- For fuel samples analysed, importance of distillation curve gradient considerable, with major impact on CTL and ATJ blending ratios
- Shallow distillation curve not necessarily inherent to CTL and ATJ-SKA production pathway
 - CTL with steep distillation curves used for ASTM certification
 - For ATJ-SKA producer states that pathway can also produce fuel meeting T50-T10 and T90-T10 requirements as neat fuel
 - May be an issue of extent of isomerisation, and hence cost of production
- Shallow curve likely inherent for ATJ-SPK, but ASTM gradient restriction perhaps not necessary
 - Distillation curve gradient restriction deliberately introduced in connection with CTL certification, to prevent combinations not covered in certification process
 - Applicability for ATJ pathway subject to debate
 - Fuel used in ATJ certification had low gradient from the onset
 - All the same, no issues observed

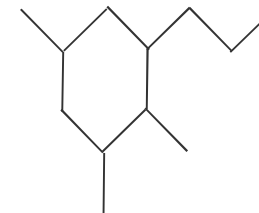
Assessment of blend ratio potential

- High biofuel blends in possible for most fuels analysed in HWWA study
- SIP limited by viscosity at -40°C
 - Achivable blend ratios 20 to 30%
 - SIP never designed for high blend ratios
- N- and iso-paraffinic fuels requiring limited addition of aromatics and cycloparaffins for blend ratios much in excess of 50%
 - Suitable components being developed by Virent / Shell
 - HDO-SK provides cycloparaffins, HDO-SAK aromatics
- ATJ-SKA and CH kerosene designed as drop-in fuels, hence in principle no blend restrictions

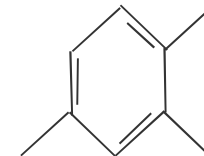


Observations on fuels not included in lab analyses

- Three fuels not included in Lab analysis since no samples were available
- Market position for HDO-SK and HDO-SAK clear
 - Intended to complement blends fuels composed of n- and iso-paraffins
 - HDO-SK provides cycloparaffins
 - HDO-SAK provides aromatics



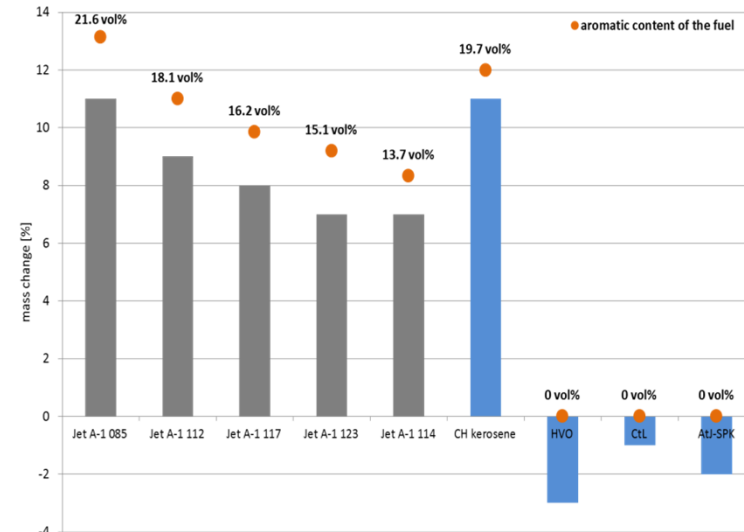
- Market position of HDCJ / Pyrolysis less clear
 - Certification oriented towards certification for binary blends with conventional fuel
 - However, aromatics content of some 50% will severely restrict blend ratios
 - Also, resulting blends will have unnecessarily high aromatics content
 - Might be better positioned to complement blends



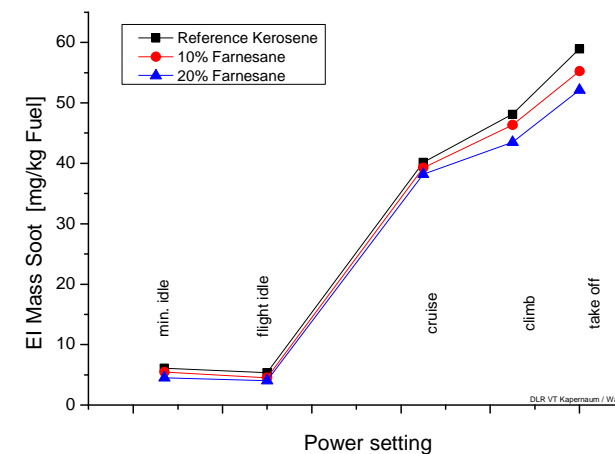
The two-faced role of aromatic compounds

- Presence of aromatic compounds required to preserve tightness of materials made from nitrile-butadiene rubber
 - Aromatics-free material not harmful in itself, but aromatics required for seal swell
 - No significant difference between HEFA, CTL and ATJ-SPK
- However, adverse effect on emissions
 - Reduction in aromatics content gives better burning fuel
 - Primarily relevant for soot emissions
- Hence, aromatics content should be limited to the minimum necessary.

Effects on mass change of NBR seals

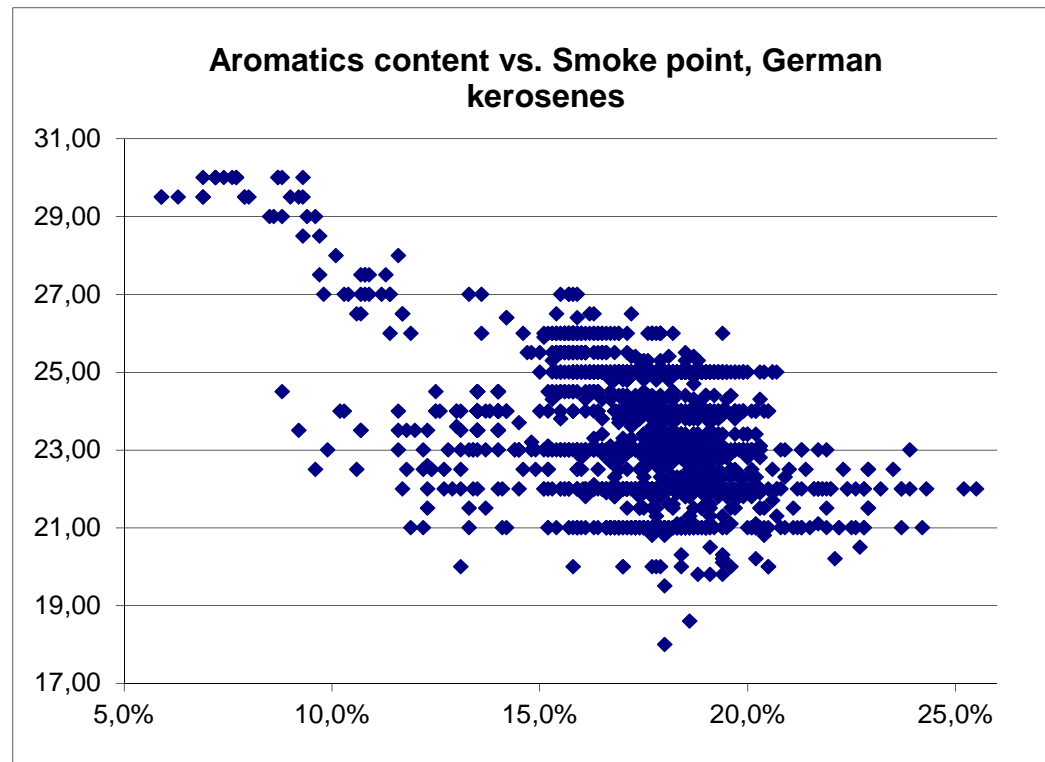


Soot Mass, in mg/kg fuel



Outlook: Further research required

- Not all aromatics are the same
 - «Aromatics» overall term for many different kinds of compounds
 - Not all aromatics have the same effect on emissions
 - Example: monoaromatics probably different from biaromatics
Ideally some aromatics may be found that produce seal swell but have little adverse effect on emissions
- Reserch on effects of different kinds of aromatics desirable



- Also, empirical determination of size of soot - contrails - climate effects desirable
 - Current estimates ranging from «as bad as all CO2 accumulated emissions from aviation together» to «not very much»
 - Makes setting of priorities difficult